

# Homogenization of both linear and nonlinear highly heterogeneous plate

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Composite plates are widely used in aeronautics applications because they offer excellent ratio between stiffness or strength performance and weight. The size of fine scale details in these heterogeneous plates is typically much smaller compared to the dimensions of the structure, thus making direct numerical analyses is prohibitively expensive. To avoid these large-scale computations, it is preferable to model these plates at the macroscale as a homogeneous continuum with effective properties obtained through a homogenization procedure. Based on asymptotic homogenization concepts (Caillerie, 1984 ; Kohn and Vogelius, 1984) discussed the homogenization of heterogeneous periodic linear elastic plates. These models are mathematically elegant and rigorous but only related to a simple engineering model (the Kirchhoff plate model). The Kirchhoff–Love plate model is the simplest and the most widely-used theory. Nevertheless this model neglects the contribution of out-of-plane stress components to the stress energy. However, when the plate slenderness ratio  $L/h$  ( $h$  is the plate thickness and  $L$  is the characteristic dimension of its mid-plane) decreases, out-of-plane stresses have an increasing influence on the plate deflection. Exactly as (Cecchi and Sab, 2007) did for Reissner-Mindlin homogenization of periodic plates, Lebée and Sab, 2012 propose a homogenization theory for their bending gradient theory (Lebée and Sab, 2011). **This method of homogenization concerns only the linear case and may be numerically implemented in order to compare this new and recent developments to our approach which is also valid in linear case (see below).** This approach correct the homogenization theory of Lewinski, 1991; Caillerie, 1984 ; Kohn and Vogelius, 1984 in order to take into account of out-of-plane stress components (transverse shearing and transverse normal stress). So they use implicitly the superposition principle and then theses theories are limited to linear elasticity.

The study of Petracca *et al.*, 2017, focused on periodic brick-masonry walls, the macro-scale behavior obeys a Reissner-Mindlin and the local heterogeneous structures is assumed to be transverse isotropic. For macroscopic Reissner-Mindlin plate model, Terada *et al.*, 2017 propose a new numerical plate testing (NPT) by adding a specific microscopic displacement terms such that the out-of-plane microscopic shear strain components, contain the macroscopic curvature associated with torsional deformation.

**In this phd thesis, for the first part we propose to implement numerically the method recently proposed by Pruchnicki 2020 (and forthcoming new theoretical development,**

**Pruchnicki (2021)) for which the macroscopic model is Nonlinear Cosserat type model. For numerical implementation of macroscopic Reissner-Mindlin (which is included model in the class of Cosserat type model) without locking we can for example refers to Krishna, 2019.** So we avoid the Saint Venant-Kirchhoff assumption considered in Coenen *et al.*, 2010; Cong *et al.*, 2015. The mechanical behaviour of the constituents of the plate is of non linear hyperelastic type (obviously we will begin with their elastic linear counterpart) . Then it is necessary to define the relation between the definitions of the macroscopic generalized strains and stresses for a plate continuum in terms of the microscopic ones. This macro-to-micro scale transition is performed by imposing the macroscopic generalized deformation gradient on the RVE (representative volume element ) through the essential boundary conditions that may be periodic conditions. Upon solution of the microstructural boundary value problem, the macroscopic generalized stress resultants are expressed by averaging the computed RVE stress field. In our work, the through thickness dimension is directly combined with the in-plane homogenization.

For the second part, we propose to work on the US School homogenization idea (Steigmann, D.J. and Pipkin, A.C) which in particular can be used to model woven fabric (two orthogonal sets of yarns interlaced with one another (Parsons *et al.* [30])). The fibers of the yarn may have elliptical, rectangular or circular cross sections. In order to model the mechanical behaviour of woven fabric, Shirani *et al.* [31] assumed that the nonlinear spatial rods are of Kirchhoff type. Nevertheless a more accurate higher order model should be considered. In the spirit of the modelling on woven fabrics (Steigmann and Pipkin [32], Steigmann and Dell’Isola [33], Shirani *et al.* [31], Steigmann [34]) and following the idea of Pipkin, we can propose new models for woven fabrics (or also classical composite plate) by using new unidimensional modelling for curved homogeneous beams (Pruchnicki *et al.* (2021)).

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